Steel Structures Congress 16-18 November 2015 "CFRP Strengthening and Rehabilitation of Corroded Steel Pipelines Under Combined Bending and Bearing"

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Introduction

- CFRP repair and strengthening of steel structures.
- Types of Corrosion.
- Traditional Methods of Repairs
- Advantageous of using CFRP
- **Laboratory Testing**
 - Cutting CFRP Sheets
 - Cleaning
 - Mixing Part A+B
 - Application to pipe surface
- Test Results
- Conclusions
- Acknowledgment
- Video ??





We need to strengthen or rehabilitate steel structures because of:

- 1. Natural disasters (such as EQ.) or man-made disasters such as road crashes
- 2. Environmental effects such as Corrosion
- 3. Increase in traffic demands or upgrades of existing buildings.



Elchalakani, M. (2004), Design of Raw Mill Stack, New Preheater, New Raw Mill, Connell Wagner, Blue Circle Cement, Waurn Ponds, Geelong, Victoria, Australia



Traditional Steel buildings Strengthening Columns Strengthening

Welding Steel Tstubs at mid-height to increase the Critical buckling load





Traditional Strengthening Steel buildings Floor and Walls Alterations - Beams and Braces





CFRP Strengthening of Steel Bridges Modern Repair Work for Steel Structures





Rehabilitation of RHS using CFRP Top, bottom and Web Surfaces-Rehabilitation



Original Section 5.0mm thick. CFRP plates location depends on the available access.

Three levels of corrosion at three different locations:
a) 20% on Top, bottom and web Plates
b) 40% on Top, bottom and web Plates
c) 60% on Top, bottom and web Plates





Test Results SME V-Wrap CFRP Strengthening of Box Girders



Journal of Thin-Walled Structures, Elsevier, UK, Vol. 57, No 1, 58-71.



Strengthening Series-Failure Modes Only the mid-span kink was observed



The failure modes observed includes;

- a) a ductile in-plane symmetric collapse mode under large bending deformation with the top flange forming a deep kink at mid-span associated with web crippling) was observed ;
- b) The mixed mode where a LTB mode formed together with a deep mid-flange kink and web crippling was not observed

c) Pure LTB mode as Le/ry is small was not observed



Rehabilitation Series-Failure Modes Only the kink and mixed mode were observed



The failure modes observed includes:

a) a ductile in-plane symmetric collapse mode under large bending deformation with the top flange forming a deep kink at mid-span associated with web crippling); was observed

b) The mixed mode where a LTB mode formed together with a deep mid-flange kink and web crippling for L=900 was observed

c) Pure LTB mode as Le/ry is small was not observed

Elchalakani, M. and Fernando D. (2014), Repair and strengthening steel RHS beams strengthened with CFRP under 3-point bending, Journal of Thin-Walled Structures, Elsevier, UK, Vol. 57, No 1, 58-71.

كلُيان التقنية العليا CFRP Strengthening of I-beam Failure Modes





specimens before testing (imperfections in S4)



lateral torsion buckling (LTB), plate end debonding



compression flange debonding



ductile symmetric collapse (forming deep kink and web crippling)



mixed mode failure (with debonding at compression and tension flange and on web)



web debonding

The failure modes observed includes;

ductile in-plane **(a)** a collapse mode symmetric bending under large deformation with the top flange forming a deep kink at mid-span associated with web crippling (S1, S2, S3 S6, SB1, SB2, SB3, STB1, STB2, STB3 and STBW6);

(b) a mixed mode where a LTB mode formed together with a mild mid-flange kink and web crippling (\$5, STBW5). Unfortunately,

(c) a pure LTB out-of-plane lateral torsion buckling ((S4, SB4, STB4),

Elchalakani, M. and Fernando D. (2012), Plastic Mechanism Analysis of unstiffened steel I-section beams strengthened with CFRP2 under 3-point bending, Journal of Thin-Walled Structures, Elsevier, UK, Vol. 57, No 1, 58-71.



Corrosion Problem of Pipelines



1.7 million km of Steel Pipelines

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Corrosion has a huge economic and environmental impact on virtually all facets of the world's infrastructure, from highways, bridges, and buildings to oil and gas, chemical processing, and water and wastewater systems. In addition to causing severe damage and threats to public safety, corrosion disrupts operations and requires extensive repair and replacement of failed assets. The annual cost of corrosion worldwide is estimated to exceed \$1.8 trillion, which translates to 3 to 4% of the Gross Domestic Product (GDP) of industrialized countries. In the US, the annual cost of corrosion is estimated as \$276B. The annual cost of corrosion to the Austi economy is estimated to be between \$36B and \$60B, whereas for the New Zealand economy the cost lies between \$5.5B and \$9.2B. Yet, governments and industries pay little attention to corrosion except in high-risk areas like aviation and maritime industries.



Corrosion

- **Result of interaction of the outer environment.**
 - WATER
 - ♦ OXYGEN
- (Exothermic reaction)
- **Formation of rust:**
 - IRON OXIDE
 - The reaction between iron and oxygen in the presence of moisture or water.

Strong acid and oxidizing agents.







Types of corrosion





Uniform corrosion





Traditional methods of repair





Advantages of using CFRP Repair

24% cheaper than welded steel sleeve repairs
73% cheaper than replacing the damaged section of the steel pipe
Short amount of time.
Undisrupted fluid transmission .
No Explosion potential.





Specimen Preparation





Carbon Fiber & Pipe Application

Carbon Fiber Sheet V-Wrap™ C200











Uses Of Carbon Fiber

Aircraft...

- Cars...
- Bicycle and Motorcycle...
- Buildings...
- Steel Beams...
- Steel Pipes...











	Corrosion	New ID	thk	tc	Lc	Lcfrp	θ	CFRP	Span	Manufacturer	Transvere Sheet	Overlap	Long Sheet	Overlap
	Level	21-Apr-14	mm	mm	mm	mm	Deg.		mm					
		T5L0C0-01	5	0	0	0	0	0	900	SME V-Wrap C200	0	0	0	0
	0%	T5L0C0-02	5	0	0	0	0	0	900	SME V-Wrap C200	0	0	0	0
		T5L0C0-03	5	0	0	0	0	0	600	SME V-Wrap C200	0	0	0	0
	Corrosion	Specimens ID	thk	tc	Lc	Lcfrp	θ	CFRP	Span	Manufacturer	Transverse Sheet	Overlap	Long Sheet	Overlap
		T4L1C0-0	4	1	100	0	360	0	900	SME V-Wrap C200	0	0	0	0
		T4L1C2-1T1L	4	1	100	300	360	1L1T	900	SME V-Wrap C200	450 x 300	150	450 x 300	150
		T4L1C2-2T2L	4	1	100	300	360	2L2T	900	SME V-Wrap C200	750 x 300	150	600 x 300	0
	20%	T4L2C0-0	4	1	200	0	360	0	900	SME V-Wrap C200	0	0	0	0
		T4L2C4-1T1L	4	1	200	400	360	1L1T	900	SME V-Wrap C200	450 x 400	150	450 x 400	150
		T4L2C4-2T2L	4	1	200	400	360	2L2T	900	SME V-Wrap C200	750 x 400	150	600 x 400	0
		T4L3C0-0	4	1	300	0	360	0	900	0	0	0	0	0
	Corrosion	Specimens ID	thk	tc	Lc	Lcfrp	θ	CFRP	Span	Manufacturer	Transverse Sheet	Overlap	Long Sheet	Overlap
		T3L1C0-0	3	2	100	0	360	0	900	SME V-Wrap C200	0	0	0	0
		T3L1C2-1T1L	3	2	100	300	360	1L1T	900	SME V-Wrap C200	450 x 300	150	450 x 300	150
		T3L1C2-1T1L-SIKA	3	2	100	300	360	1L1T	900	SIKA 300C Wrap	450 x 300	150	450 x 300	150
	40%	T3L2C0-0	3	2	200	0	360	0	900	SME V-Wrap C200	0	0	0	0
		T3L2C4-1T1L	3	2	200	400	360	1L1T	900	SME V-Wrap C200	450 x 400	150	450 x 400	150
		T3L2C4-1T1L-SIKA	3	2	200	400	360	1L1T	900	SIKA 300C Wrap	450 x 400	150	450 x 400	150
		T3L3C0-0	3	2	300	0	360	0	900	0	0	0	0	0
	Corrosion	Specimens ID	thk	tc	Lc	Lcfrp	θ	CFRP	Span	Manufacturer	Transverse Sheet	Overlap	Long Sheet	Overlap
		T2L1C0-0	2	3	100	0	360	0	900	SME V-Wrap C200	0	0	0	0
		T2L1C2-1T1L	2	3	100	300	360	1L1T	900	SME V-Wrap C200	450 x 300	150	450 x 300	150
		T2L1C2-1T1L-SIKA	2	3	100	300	360	1L1T	900	SIKA 300C Wrap	450 x 300	150	450 x 300	150
	60%	T2L2C0-0	2	3	200	0	360	0	900	SME V-Wrap C200	0	0	0	0
		T2L2C4-1T1L	2	3	200	400	360	1L1T	900	SME V-Wrap C200	450 x 400	150	450 x 400	150
		T24L2C4-1T1L-SIKA	2	3	200	400	360	1T1L	900	SIKA 300C Wrap	450 x 400	150	450 x 400	150
		T2L3C0-0	2	3	300	0	360	0	900	SIKA 300C Wrap	0	0	0	0
	Corrosion	Specimens ID	thk	tc	Lc	Lcfrp	θ	CFRP	Span	Manufacturer	Transverse Sheet	Overlap	Long Sheet	Overlap
		T1L1C0-0	1	4	100	0	360	0	900	SME V-Wrap C200	0	0	0	0
		T1L1C2-1T1L	1	4	100	300	360	1L1T	900	SME V-Wrap C200	450 x 300	150	450 x 300	150
		T1L1C2-2T2L	1	4	100	300	360	2L2T	900	SME V-Wrap C200	750 x 300	150	600 x 300	0
	80%	T1L2C0-0	1	4	200	0	360	0	900	SME V-Wrap C200	0	0	0	0
		T1L2C4-1T1L	1	4	200	400	360	1L1T	900	SME V-Wrap C200	450 x 400	150	450 x 400	150
		T1L2C4-2T2L	1	4	200	400	360	2L2T	900	SME V-Wrap C200	750 x 400	150	600 x 400	0
		T1L3C0-0	1	4	300	0	360	0	900	0	0	0	0	0





Specimens Lc/D=8.0

		_	Corrosion	New ID	thk	tc	Lc	Lcfrp	θ	CFRP	Span	Manufacturer	Transvere Sheet	Overlap	Long Sheet	Overlap	Application	
				21-Apr-14	mm	mm	mm	mm	Deg.		mm							Î
				ST4L8C8-0	4	1	800	0	360	0	900	SME V-Wrap C200	0	0	0	0	0	
													1 x 750 x 600 +					
		1.000	20%	ST4L8C8-2T2L	4	1	800	800	360	2L2T	900	SME V-Wrap C200	1 x 350 x 750	150	600 x 800	0	2L2T	1
													2 x 750 x 600 +					
		100		ST4L8C8-4T4L	4	1	800	800	360	4L4T	900	SME V-Wrap C200	2 x 350 x 750	150	2 x 600 x 800	0	2L2T2L2T	
			Corrosion	Specimens ID	thk	tc	Lc	Lcfrp	θ	CFRP	Span	Manufacturer	Transverse Sheet	Overlap	Long Sheet	Overlap		
in in				ST3L8C8-0	3	2	800	0	360	0	900	SME V-Wrap C200	0	0	0	0	0	
													1 x 750 x 600 +					
		100	40%	ST3L8C8-2T2L	3	2	800	800	360	2L2T	900	SME V-Wrap C200	1 x 350 x 750	150	600 x 800	0	2L2T	
間	Seattle Burst												2 x 750 x 600 +					
				ST3L8C8-4T4L	3	2	800	800	360	4L4T	900	SME V-Wrap C200	2 x 350 x 750	150	2 x 600 x 800	0	2L2T2L2T	
1			Corrosion	Specimens ID	thk	tc	Lc	Lcfrp	θ	CFRP	Span	Manufacturer	Transverse Sheet	Overlap	Long Sheet	Overlap	Overlap	
				ST2L8C8-0	2	3	800	0	360	0	900	SME V-Wrap C200	0	0	0	0	0	
and the second second	and the second												1 x 750 x 600 +					
			60%	ST2L8C8-2T2L	2	3	800	800	360	2L2T	900	SME V-Wrap C200	1 x 350 x 750	150	600 x 800	0	2L2T	ļ
													2 x 750 x 600 +					
-	ANT ANT AND			ST2L8C8-4T4L	2	3	800	800	360	4L4T	900	SME V-Wrap C200	2 x 350 x 750	150	2 x 600 x 800	0	2L2T2L2T	
C-G-MSER	aluga and a		Corrosion	Specimens ID	thk	tc	Lc	Lcfrp	θ	CFRP	Span	Manufacturer	Transverse Sheet	Overlap	Long Sheet	Overlap	Overlap	
in the	The second			ST1L8C8-0	1	4	800	0	360	0	900	SME V-Wrap C200	0	0	0	0	0	
	An office												1 x 750 x 600 +					1
1000	S-IT		80%	ST1L8C8-2T2L	1	4	800	800	360	2L2T	900	SME V-Wrap C200	1 x 350 x 750	150	600 x 800	0	2L2T	
and a										1			2 x 750 x 600 +					
				ST1L8C8-4T4L	1	4	800	800	360	4L4T	900	SME V-Wrap C200	2 x 350 x 750	150	2 x 600 x 800	0	2L2T2L2T	
											Lcfrp]						







The total number of specimens is 43





The total number of specimens is 43





Mechanical Properties of CFRP

	Manufa	acturer	Sika Plates CarboDur S	Sika Sikadur 330 Sheets	Structural Tech C180 V-Wrap		
		Mean Value	165,000 N/mm ²	230,000 N/mm ²	227,000 N/mm ²		
dulues		Min Value	> 160,000 N/mm ²	> 230,000 N/mm ²	> 227,000 N/mm ²		
E-Mo		5% Fractile Value	162,000 N/mm ²	230,000 N/mm ²	227,000 N/mm ²		
		95% Fractile Value	180,000 N/mm ²	230,000 N/mm ²	227,000 N/mm ²		
		Mean Value	3,100 N/mm ²	3,500 N/mm ²	4,000 N/mm ²		
rength		Min Value	> 2,800 N/mm ²	> 3,500 N/mm ²	4,000 N/mm ²		
sile St		5% Fractile Value	3,000 N/mm ²	3,500 N/mm ²	4,000 N/mm ²		
Ten		95% Fractile Value	3,600 N/mm ²	3,500 N/mm ²	4,000 N/mm ²		
	Stain at Brea	k* (Min Value)	> 1.70%	> 1.5%	> 1.70%		
	Thickne	ess (mm)	1.2	0.13	0.28		

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Prepare Carbon Fiber





Pipe Application...















Sanding







Grinding



Adhesive Mixing



Mixing Part A



Adhesive Mixing





Prepare The Surface Area



Preparing



Carbon Saturated



Saturated

Transverse











Why Transverse & Longitude Direction?

Transverse Direction

Longitude Direction



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2. Laboratory Testing









Failure Modes

CFRP System
Fibre Fracture
Local Buckling
Intermediate Plate Debonding
Steel Pipe
Steel Fracture
Local Buckling



3. Test Results



Specimens after Testing





Gain in Strength due to CFRP



% All around 360 Deg Thickness Corrosin



Structural Technology wrapping System Provided higher strength





Effect of the corrosion length (L_c) on the normalised strength (% P_u / $P_{u,control}$)





Load-deflection Curves





Load-deflection Curves



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Design Method for Repair System Under Combined Bending and Bearing





Conclusions

The results showed that the combined flexural and bearing strength of the repaired steel pipelines can be significantly increased by adhesively bonding CFRP.

The percent increase in strength was mostly affected by the corrosion level where the maximum gain was 434% which was obtained for the most severe 30% corrosion in the wall thickness. The average increase in the load carrying capacity was 97% and 169% for the rehabilitation and strengthening series, respectively.

The stiffness and capacity of the un-corroded control specimen was fully restored for the repaired specimens with 20% corrosion in the wall. However, for higher levels of corrosion of 40% to 80% such stiffness and capacity were not fully restored. Thus adding more CFRP sheets in the circumferential and longitudinal directions may restore the un-corroded stiffness and capacity for 40% to 80% corrosion.

Design equations based on the bare and composite section properties were derived to predict the strength of bare and repaired CHS using CFRP under combined bending and bearing. The author would like to thank Dr. Tarek Alkhrdaji and Mr Christian Hill of "Structural Technologies" for providing the CFRP sheets and for the kind support for our ongoing research.

The assistance and support of Sika staff in particular Mr Rob Bonnici and Eng Imad is greatly appreciated.

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