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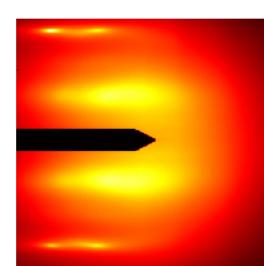


Radar Screening using Weekly Ionized Plasmas

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Contents

- Stealth Planes, Context and the Original Idea
- Defining the (Active) Stealth Problem
- Plasma Screening Model (for a Weakly Conductive Plasma)
- The Rate Equation and Solution for a Plasma Flow
- Simulations for Incompressible and Compressible Flows
- Some New Results for the Hypersonic Regime
- Summary + Q & A

Stealth Planes

- Horton brothers develop first flying wing concept in 1930s
- Observe that the radar cross section is significantly reduced







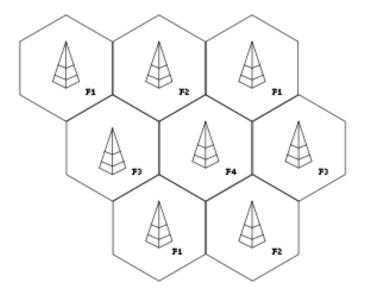
Stealth Planes are not Invulnerable



March 27, 1999, 250th Serbian Air Deference Brigade shoot down an American F-117 Nighthawk for the first and only time (to-date).

How did they do it?

First application of Cellular Networks for air defense against stealth planes!!





Context



Original Idea

- A LEDROC 31700 THE REPORT OF A LEDROC 31700 THE REPORT OF A LEDROC ALL TO A
- A. Eldredge while working for General Electric

First proposed in 1956 by

- US patent* granted in 1964
- Proposed using a particle accelerator in an aircraft to create a cloud of ionised gas that would '...absorb incident radar beams'

*A. Eldredge, *Object Camouflage Method and Apparatus*, US Patent No. 3127608, August 6, 1956; Issued on March 31, 1964.

What do we need to understand?

Principles of
RadarPrinciples of
Fluid Dynamics

Principles of Plasma Physics

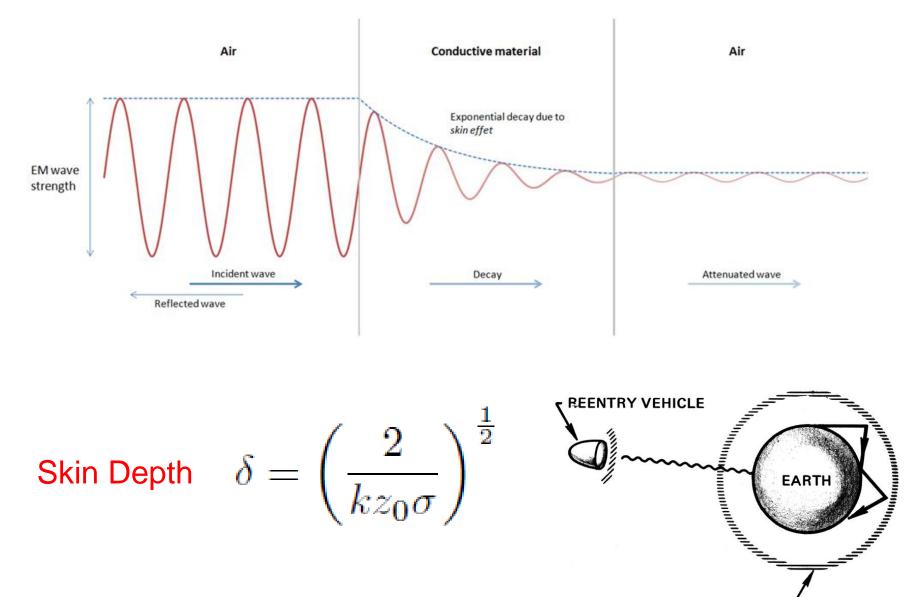
Defining the (Active) 'Stealth Problem'

Given Maxwell's equations, find functions of space for the <u>permittivity</u> and <u>conductivity</u> which can 'fly' such that the reflected microwave energy is effectively zero.

Generic Approaches

- Consider functions which reflect energy away from transmitter
- Consider materials that absorb microwave radiation

Conductors and EM waves



Z IONOSPHERE

Plasma Screening Model

Impulse Response Function for a <u>weakly conductive plasma</u> is

$$f(t) = -z_0 \frac{d}{dt} [\sigma(t) \exp(-\sigma_0 t/\epsilon_0)]$$

- For a weakly ionized plasma, the electron number density determines its conductivity.
- In terms of this result, there are two principal factors affecting the performance of a practical radar plasma screening system:
 - maximizing the electron number density of the plasma;
 - maximizing the thickness of the screen.

Radar Screening Skin Depth

 For 1 cm wavelength microwaves, the weakly conductive plasma condition gives

$$\sigma_0 << 17$$

• Skin depth is

$$\delta = \frac{10^{-3}}{\sqrt{\sigma_0}}$$

 For plasma with conductivity of 1 siemens/meter, the skin depth is 1mm, i.e. electric field strength decays by 63% over 1mm penetration into plasma sheath.

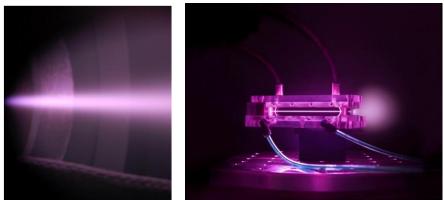
The Rate Equation

 For a weakly ionized plasma the conductivity is proportional to the electron number density

 Required to simulate the electron number density generated for a plasma screening system

• Rate equation is

0



$$\frac{\partial n}{\partial t} = D\nabla^2 n + In + B - Rn^2$$

Diffusion + Ionization + Beam + Recombination

Plasma Flow: Sub-sonic Case

• For a moving aerospace vehicle with velocity v the plasma density conforms to the conservation equation

$$\frac{\partial n}{\partial t} = \nabla \cdot (n\mathbf{v})$$

• Required to solve the steady state equation

$$D\nabla^2 n + B + In - Rn^2 - \nabla \cdot (n\nabla u) = 0$$

where *u* is the velocity potential obtained by solving

$$abla^2 u = 0$$
 Incompressible Flow

Iterative Solution

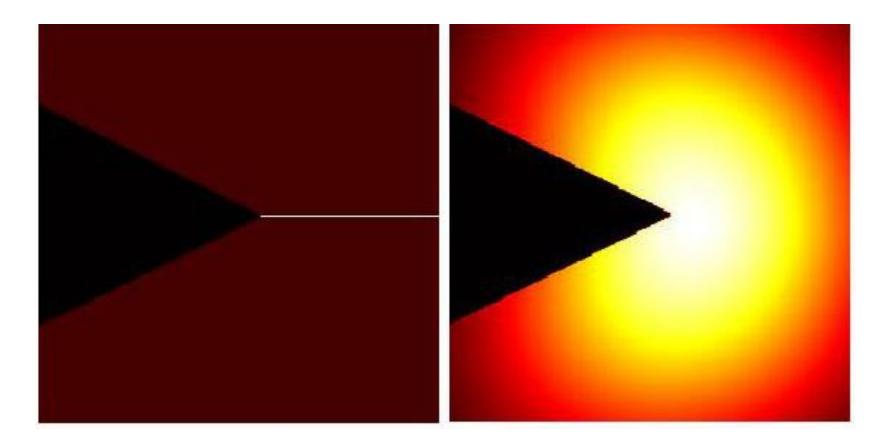
For
$$\nabla \cdot (u\nabla n) = 0$$

 $n = \frac{1}{4\pi r} \otimes \left(\frac{B}{u+D} + \frac{In}{u+D} - \frac{Rn^2}{u+D}\right)$ Fundamental equation with no frills
• Electron generation $n_1 = \frac{1}{4\pi r} \otimes \frac{B}{u+D}$
• Ionization $n_2 = n_1 + \frac{1}{4\pi r} \otimes \frac{In_1}{u+D}$

Recombination $n_3 = n_1 + n_2 - \frac{1}{4\pi r} \otimes \frac{Rn_2^2}{u+D}$

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2D simulation of an e-beam induced plasma sheath for the subsonic case



Electron Beam

Electron Number Density

Compressible Flow Regime

What is the effect of a plasma screen generated at super-sonic velocities?

• Number Density Equation

$$n = \frac{1}{4\pi r} \otimes \left(\frac{B}{u+D} + \frac{In}{u+D} - \frac{Rn^2}{u+D}\right)$$

• Velocity Potential is the solution of

$$\left((1-M^2)\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2}\right)u(x,y,z) = 0$$

where *M* is the Mach number of the incoming free stream

Incorporating Shock Waves

• Wave Velocity Potential given by the solution of the wave equation (for sound speed *c*)

$$\left(\nabla^2 - \frac{1}{c^2}\frac{\partial^2}{\partial t^2}\right)u = s$$

where s is the source function (surface of aerofoil)

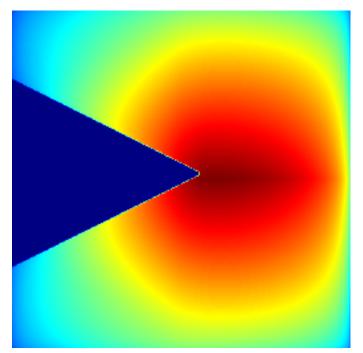
2D Fresnel Zone (for frequency *f* and distance from source *L*)

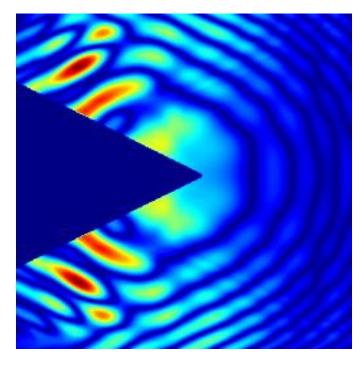
$$u(\mathbf{r}) \sim \frac{1}{4\pi L} |\exp(i\alpha r^2) \otimes s(\mathbf{r})|, \ \alpha = \frac{\pi f}{cL}$$

Combined Potential Flow in 2D

Combined velocity potential is given by

Compressible Velocity Potential + Wave Velocity Potential



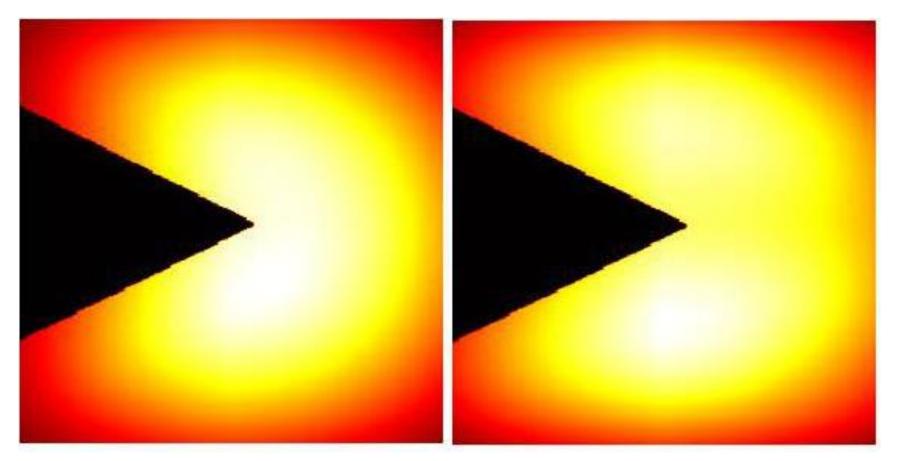




Compressible Flow Velocity Potential

Wave Velocity Potential

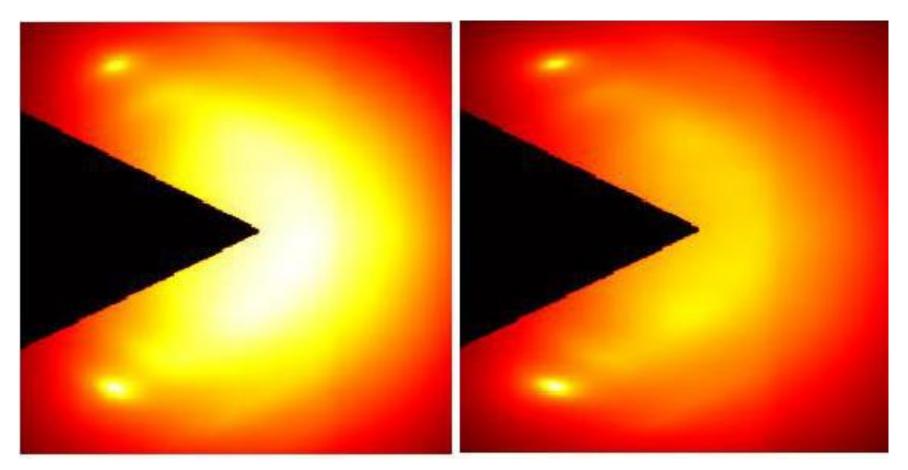
2D simulation of an e-beam induced plasma sheath for the supersonic case



Electron Number Density for M=2

Electron Number Density for M=3

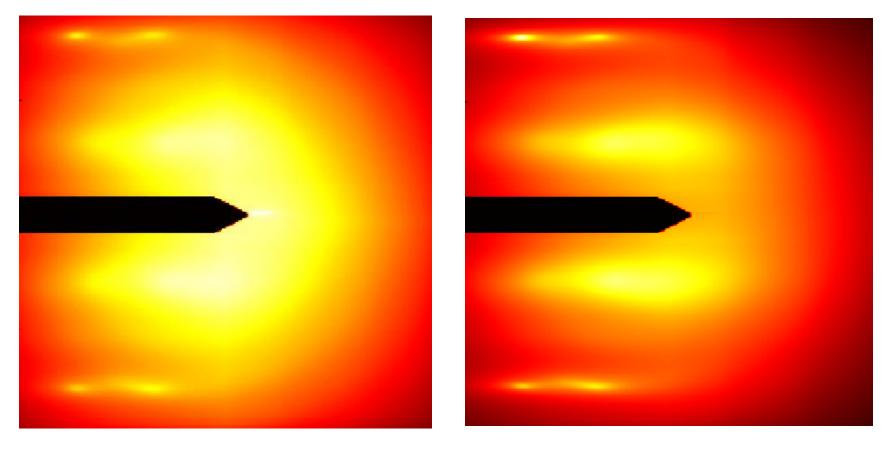
Q3D Simulation of an e-beam induced plasma sheath for the supersonic case



Electron Number Density for M=2

Electron Number Density for M=3

Q3D Simulation of an e-beam induced plasma sheath for the hypersonic case



Electron Number Density for M=3

Electron Number Density for M=6

Summary

• The *Radar Cross Section* can be significantly reduced with weakly ionized plasmas for which the *Impulse Response Function* (IRF) is

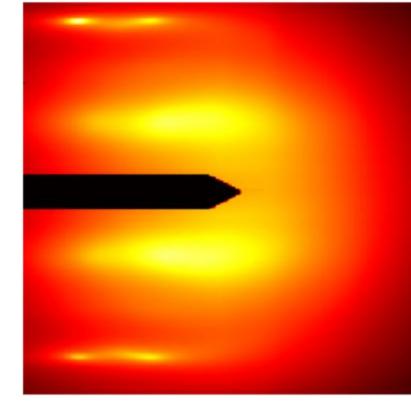
$$\frac{d}{dt}[\sigma(t)\exp(-\sigma_0 t/\epsilon_0)]$$

 The IRF is characterised by a negative exponential determined by the conductivity of the plasma sheath

• For a weakly ionized plasma, the conductivity is proportional to the electron number density which is computed by solving the equation

$$n = \frac{1}{4\pi r} \otimes \left(\frac{B}{u+D} + \frac{In}{u+D} - \frac{Rn^2}{u+D}\right)$$





Publication:

J M Blackledge and A Kawalec **Steady State Solutions for a Weakly Ionised Plasma in a Sub- and Super-Sonic Axial Flow** MATHEMATICA AETERNA, Vol. 4, No. 2, 143 - 162, 2014. <u>http://www.e-hilaris.com/MA/2014/MA4_2_7.pdf</u>



